

## Design options for radiation tolerant microstrip sensors for the CBM Silicon Tracking System (STS)\*

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The expected neutron fluence for the CBM STS is  $1 \times 10^{14} \text{ n}_{eq} \text{ cm}^{-2}$ , after which an upgrade of sensors is foreseen. The main impact of radiation damage is the loss in the charge collection efficiency (CCE) limited by the breakdown voltage  $V_{bd}$ . Also we aim to minimize the capacitive noise. The dominant contributor to the capacitive noise comes from the interstrip capacitance  $C_{int}$ . To summarize, we aim to develop microstrip detectors having low  $C_{int}$ , high  $V_{bd}$  and maximum CCE.

### Fluence Profile

Table 1 shows the expected neutron fluence for five years of required CBM runtime. In this table, the initial resistivity of silicon has been taken to be  $5.33 \text{ K}\Omega\text{-cm}$ , the lifetimes of electrons  $\tau_e$  and holes  $\tau_h$  have been calculated using Kramberger's model [1] assuming an operating temperature of  $-10^\circ\text{C}$ . One can observe a deterioration of carrier life time with fluence which will have an impact on the CCE, especially on the p-side since this side collects less mobile holes.

Table 1: Fluence profile of neutrons for the CBM STS.

Year	Fluence ( $\text{n}_{eq} \text{ cm}^{-2}$ )	$N_{eff}$ ( $\text{cm}^{-3}$ )	$\tau_e$ (ns)	$\tau_h$ (ns)	$V_{fd}$ (V)
1	$2 \times 10^{13}$	$2.8 \times 10^{11}$	1140	1050	28
2	$4 \times 10^{13}$	$-1.54 \times 10^{11}$	570	527	20
3	$6 \times 10^{13}$	$-5.35 \times 10^{11}$	380	351	44
4	$8 \times 10^{13}$	$-8.84 \times 10^{11}$	285	263	75
5	$1 \times 10^{14}$	$-12.1 \times 10^{11}$	228	211	100

### Strip Isolation

In order to investigate the life time of sensors, it is imperative to extract the CCE as a function of fluence for which one has to understand the strip isolation in particular on the ohmic side. Hence various isolation techniques have been explored both through prototyping as also through simulations, for example P-stop, P-Spray, Modulated P-spray (conventional isolation techniques) and also a new isolation technique, the Schottky barrier. Schottky barrier can be defined either through metal work function value or through barrier height which in turn depends on the substrate type and the metal used for Schottky contact. For Aluminum, the barrier height is  $0.72 \text{ eV}$  for n-type silicon while for p-type silicon, the barrier height is  $0.58 \text{ eV}$  [2]. A comparison of the conventional isolation techniques with Schottky barrier in terms of  $V_{bd}$ ,  $C_{int}$  and CCE is shown in Table 2. One can infer that the Schottky barrier is the best choice

in terms of  $V_{bd}$  and  $C_{int}$ . However in terms of CCE, the Schottky barrier gives the worst performance especially after type-inversion. Therefore, Schottky barrier has not been opted as a suitable isolation technique. Besides P-stop and P-spray, another isolation technique namely modulated P-spray has also been explored. An optimization of modulated P-spray has been performed. It has been found that using a moderate P-stop width of around  $15 \mu\text{m}$  and very low P-spray concentration of around  $1 \times 10^{15} \text{ n}_{eq} \text{ cm}^{-3}$  gives the best performance in terms of  $V_{bd}$  and  $C_{int}$ , referred to as Optimized Modulated P-spray in Table 3. Finally a comparison of P-stop, P-spray and Optimized Modulated P-spray after one year of operation and the maximum fluence expected at the end of five years of CBM run is shown in Table 3. One can notice from this table that using Optimized Modulated P-spray, the  $V_{bd}$  has increased by around 60% and  $C_{int}$  has reduced by 25% while maintaining the same CCE as with conventional isolation techniques. In Tables 2 and 3,  $V_{bd}$ ,  $C_{int}$  and CCE are simulated values confirmed with measurements. Hence Optimized Modulated P-spray is the best choice for isolation technique in terms of  $V_{bd}$ ,  $C_{int}$  and CCE.

Table 2: Comparison of conventional isolation techniques with Schottky barrier.

Isolation Technique	Fluence ( $\text{n}_{eq} \text{ cm}^{-2}$ )	$V_{bd}$ (V)	$C_{int}$ ( $\text{pF cm}^{-1}$ )	CCE (%)
P-stop	$3.93 \times 10^{12}$	1010	2.1	91.25
	$20.60 \times 10^{12}$	890	2.29	86.25
P-spray	$3.93 \times 10^{12}$	524	2.6	93
	$20.60 \times 10^{12}$	450	2.7	86.25
Schottky Barrier	$3.93 \times 10^{12}$	1450	2.05	79
	$20.60 \times 10^{12}$	1350	1.80	77.5

Table 3: Comparison between p-stop, p-spray and optimized modulated p-spray at low and high fluence.

Isolation Technique	Fluence ( $\text{n}_{eq} \text{ cm}^{-2}$ )	$V_{bd}$ (V)	$C_{int}$ ( $\text{pF cm}^{-1}$ )	CCE (%)
P-stop	$2 \times 10^{13}$	980	2.02	93.15
	$1 \times 10^{14}$	720	2.03	88.87
P-spray	$2 \times 10^{13}$	513	2.56	93.17
	$1 \times 10^{14}$	495	2.44	89
Opt. Mod. P-spray	$2 \times 10^{13}$	1600	1.58	93.22
	$1 \times 10^{14}$	1150	1.60	89

### References

- [1] V.Cindro et. al., *IEEE Trans. Nucl. Sci.* N09-2, pp.139-142, 2006.
- [2] [http://www.pfk.ff.vu.it/lectures/funkc\\_dariniai/diod/schottky.htm](http://www.pfk.ff.vu.it/lectures/funkc_dariniai/diod/schottky.htm).

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